

## RADIUSI O'ZGARUVCHAN, DOIRAVIY, QOVUSHOQ-ELASTIK STERJENNING BURALMA TEBRANISH MASALASI TENGLAMALARI

**Baxtiyor Iskandarovich Ashurov**  
Samarqand iqtisodiyot va servis instituti  
[ashrovbakhtiyor89@gmail.com](mailto:ashrovbakhtiyor89@gmail.com)

### ANNOTATSIYA

Ushbu maqola doirasida radiusi o'zgaruvchan sterjenning buralma tebranish tenglamalarini keltirib chiqaramiz. Bunda qobiqning ko'ndalang kesimi doiraviy bo'lsin deb, shuningdek uning materialini qovushoq-elastik deb hisoblaymiz.

**Kalit so'zlar:** interrodifferensial, qovushoq-elastik, radial, modifitsirlangan,

### ABSTRACT

In this article, the equations of torsional vibrations of a rod of variable radius are derived. In this case, the cross section of the shell is considered round, and its material is viscoelastic.

**Keywords:** interdifferential, viscoelastic, radial, modified.

### KIRISH

Qaralayotgan masala  $\sigma_{r\theta} - F'(z)\sigma_{z\theta} = \Delta f_{nS_1}(z, t)$ . chegaraviy va nolga teng

boshlang'ich shartlarda  $M_0(\Delta_0\Psi_1) - \frac{1}{b^2} \frac{\partial^2\Psi_1}{\partial t^2} = 0$ ;  $0 \leq r \leq R$  interrodifferensial

tenglamani integrallashga keltiriladi. Keltirilgan harakat tenglamasidan ko'rinadiki, qaralayotgan doiraviy sterjenning buralma tebranishlarida uning kuchlanganlik-deformatsiyalanganlik holati faqat va faqat  $\Psi_1$  potentsialdangina bog'liq bo'lishi kerak. Kuchlanganlik-deformatsiyalanganlik holatining bu potentsialga bog'liq bo'lmagan boshqa parametrlari nolga aylanishlari kerak. Birinchi paragraf natijalariga ko'ra  $U_\theta = -\frac{\partial\Psi_1}{\partial r}$  va  $\sigma_{r\theta} = M \left[ \frac{1}{r} \frac{\partial}{\partial r} - \frac{\partial^2}{\partial r^2} \right] \Psi_1$ ,  $\sigma_{z\theta} = -M \frac{\partial^2\Psi_1}{\partial r\partial z}$ . formulalar bilan aniqlanuvchi  $U_\theta$ ,  $\varepsilon_{z\theta}$ ,  $\varepsilon_{r\theta}$ ,  $\sigma_{z\theta}$ ,  $\sigma_{r\theta}$  kattaliklar  $\Psi_1$  potentsialdan bog'liq va faqat shu kattaliklargina noldan farqlidirlar.

### ADABIYOTLAR TAHLILI VA METODOLOGIYA

1. Амензаде Ю.А. Теория упругости –Deformatsiyalanganlik holati o'rganilgan.
2. Болотин В.В. Колебания и устойчивость упругой цилиндрической оболочки в потоке сжимаемого газа – radiusi o'zgaruvchan silindirik jism ichida suyuqlik harakati o'rganilgan.
3. Ляв А. Математическая теория упругости- Diffirensial tenglamalar orqali suyuqlik holati o'rganilgan.
4. Никифоров А.Ф.-suyuqlik holati radiusi o'zgaruvchan silindirik idish ichida o'rganilgan.
5. Петрашень Г.И. Проблемы инженерной теории колебаний вырожденных систем –deformatsiyalanuvchi jism holati o'rganilgan.
6. Филиппов И.Г, Худойназаров Х.Х. Уточнение уравнений продольно-радиальных колебаний круговой цилиндрической вязкоупругой оболочки – radiusi o'zgaruvchansilindirik idish ichida suyuqlik holati o'rganilgan.
7. Филиппов И.Г., Чебан В.Г. Математическая теория колебаний упругих и вязкоупругих пластин и стержней. – radiusi o'zgaruvchansilindirik idish ichida suyuqlik holati o'rganilgan.
8. Худойназаров Х.Х. Нестационарное взаимодействие круговых цилиндрических упругих и вязкоупругих оболочек и стержней с деформируемой средой. – radiusi o'zgaruvchansilindirik idish ichida suyuqlik holati o'rganilgan.
9. Худойназаров Х.Х., Абдирашидов А. Нестационарное взаимодействие упругопластически деформируемых элементов конструкций с жидкостью. – radiusi o'zgaruvchansilindirik idish ichida suyuqlik holati o'rganilgan.

## МУНОКАМА

Buralma tebranish tenglamalari qaralayotgan doiraviy sterjenniki bo'lganliklari uchun uning nuqtalarining ko'chishlari bo'lgan  $U_{\theta}$  larning bosh qismlarini ajratamiz. Buning uchun  $U_{\theta}^{(0)}(r)$  funksiyaning  $U_{\theta}^{(0)} = -\beta B I_1(\rho r)$  ifodasiga kiruvchi  $I_1(\beta r)$  Besselning modifitsirlangan funksiyasini  $r$ - radial koordinataning darajalari bo'yicha darajali qatorga yoyamiz. U holda  $U_{\theta}^{(0)}(r)$  funksiya uchun quyidagi formulaga ega bo'lamiz:

$$U_{\theta}^{(0)}(r) = -\sum_{n=0}^{\infty} \beta^{2n+2} \cdot B \frac{\left(\frac{r}{2}\right)^{2n+1}}{n!(n+1)!}$$

Ma'lumki qobiqlar va plastinalar nazariyalarida asosiy izlanuvchi o'zgaruvchilar sifatida qobiq yoki plastina o'rta sirti nuqtalarining ko'chishlari qabul qilanadi. [1, 2, 3, 11, 14]. Ammo, bunday qilinganida qobiqning qalinligi bo'yicha chetki yoki unga yaqin nuqtalarining ko'chishlarini topib bo'lmaydi. Bunday holda qo'shimcha gipoteza kiritadilar, ya'ni qobiqning o'rta sirtidan boshqa sirlari nuqtalarining ko'chishlari o'rta sirt nuqtalari ko'chishi  $W_0$  bilan biror chiziqli  $kz$  funksiyaning yig'indisidan iborat bo'lsin deb faraz qiladilar. Formula tilida ushbu gipoteza

$$W = W_0 \pm kz$$

ko'rinishda bo'ladi. Bu yerda  $k$ -o'zgarimas koeffitsiyent;  $z$  - qobiqning normali bo'ylab yo'nalgan o'zgaruvchi. Bu o'zgaruvchining boshlang'ich nuqtasi o'rta sirt ustida deb hisoblanadi.

Umuman olganda asosiy izlanuvchi kattaliklar sifatida qobiq o'rta sirti nuqtalarining ko'chishlarini tanlash yagona yo'l emas. Masalan, izlanuvchi funksiyalar sifatida qobiqning shunday sirti nuqtalarning ko'chishlarini qabul qilish mumkinki, bu sirt  $r \rightarrow 0$  bo'lgan limitik holatda sterjen o'rta chizig'i yoki qobiqning ichki  $r=r_1$  va yoki tashqi  $r=r_2$  sirtlariga o'tsin. Bunday "harakatlanuvchi" sirt nuqtalarning ko'chishlari asosiy izlanuvchi kattaliklar sifatida qabul qilingan holda kontakt masalalarida kontakt shartlarini aniq qo'yish mumkin bo'ladi.

Yuqorida bayon qilingan fikrlar bilan bo'g'liq ravishda [8] asosiy sirt sifatida silindrik qobiqning radiusi

$$\xi = \frac{r_1}{2} \left( x - \frac{r_1}{r_2} \right)$$

formula bilan aniqlanuvchi biror "oraliq" sirtini qabul qilingan. Bu yerda  $x$  o'zgarimas son va u quyidagi tengsizlikni qanoatlantiradi.

$$2 + \frac{r_1}{r_2} \leq x \leq 2 \frac{r_2}{r_1} + \frac{r_1}{r_2}$$

Ta'kidlash lozimki, kiritilgan  $x$  o'zgarimasning

$$2 + \frac{r_1}{r_2}; \quad 1 + \frac{r_2}{r_1} + \frac{r_1}{r_2}; \quad 2 \frac{r_2}{r_1} + \frac{r_1}{r_2}$$

larga teng bo'lgan qiymatlarida  $\xi = \frac{r_1}{2} \left( x - \frac{r_1}{r_2} \right)$  formula bilan aniqlangan

"oraliq" sirt radiusi  $-\xi$  quyidagi qiymatlarni qabul qiladi (mos ravishda):

$$r_1; \quad \frac{r_1 + r_2}{2}; \quad r_2.$$

Bundan ko'rinadiki tanlangan "oraliq" sirti qobiqning ichki ( $\xi = r_1$ ), o'rta ( $\xi = \frac{r_1 + r_2}{2}$ ) yoki tashqi ( $\xi = r_2$ ) sirtlariga o'tadi. Yuqorida ta'kidlangan limitik holda, ya'ni  $r_1 = 0$  bo'lganda silindrik qobiq doiraviy sterjenga o'tadi. Bu holda "oraliq" sirt esa sterjenning o'q ( $\xi = 0$ ) chizig'iga aylanadi.

Biz qarayotgan masalada qobiq o'rnida sterjen kelmoqda. Shuning uchun asosiy sirt sifatida biz radiusi  $r = R$  bo'lgan sirtni qabul qilamiz. Ya'ni bu holda  $\xi = \frac{r_1}{2} \left( x - \frac{r_1}{r_2} \right)$  formula bilan aniqlanuvchi radius  $R$  ga teng, boshqacha aytganda

$\xi = R$ . Shuning uchun  $U_{\theta}^{(0)}(r) = -\sum_{n=0}^{\infty} \beta^{2n+2} \cdot B \frac{\left(\frac{r}{2}\right)^{2n+1}}{n!(n+1)!}$  formulaga  $r = R$  qiymatni qo'yamiz va almashtirilgan  $U_{\theta}^{(0)}(r)$  -ko'chishning bosh qiymatlarini qaraymiz. Bu bosh qism qatorning birinchi hadiga teng. Uni  $U_{\theta,0}^{(0)}$  orqali belgilab

$$U_{\theta,0}^{(0)} = -\frac{1}{2} \beta^2 B.$$

ifodaga ega bo'lamiz. Oxirgi  $U_{\theta,0}^{(0)} = -\frac{1}{2} \beta^2 B$  formulani hisobga olsak

$U_{\theta}^{(0)}(r) = -\sum_{n=0}^{\infty} \beta^{2n+2} \cdot B \frac{\left(\frac{r}{2}\right)^{2n+1}}{n!(n+1)!}$  ifoda  $r = R$  va  $n = 0$  bo'lganda

$$U_{\theta}^{(0)}(r) = R U_{\theta,0}^{(0)}$$

ko'rinishni oladi. Bu yerdan ko'rinadiki yangidan kiritilgan  $U_{\theta,0}^{(0)}$  - funksiya deformatsiya o'lchamiga (o'lchamsiz) ega ekan.

## NATIJALAR

Endi bu ishlar bajarilgach chegaraviy shartlarni almashtirishga o'tamiz. Buning

uchun  $\sigma_{r\theta} - F'(z)\sigma_{z\theta} = \Delta f_{nS_1}(z, t)$ . shartga  $f_{nS_1}(z, t) = \int_0^{\infty} \frac{\sin kz}{-\cos kz} \left. dk \int_{(l)} f_{nS_1}^{(0)}(k, p) e^{pt} dp \right\}$ ,

va  $\sigma_{r\theta}(r, z, t) = \int_0^{\infty} \frac{\sin kz}{-\cos kz} \left. dk \int_{(l)} \sigma_{r\theta}^{(0)}(r, k, p) e^{pt} dp \right\}$ ,

$$\sigma_{z\theta}(r, z, t) = \int_0^{\infty} \frac{\cos kz}{\sin kz} \left. \right\} dk \int_{(l)} \sigma_{z\theta}^{(0)}(r, k, p) e^{pt} dp, \text{ almashtirishlarni qo'llaymiz va}$$

$$\sigma_{r\theta}^{(0)} - F'(z)\sigma_{r\theta}^{(0)} = \Delta f_{nS_1}^{(0)}(k, p), \quad r = F(z)$$

Chegaraviy shartga ega bo'lamiz. Ushbu  $\sigma_{r\theta} - F'(z)\sigma_{z\theta} = \Delta f_{nS_1}(z, t)$ .

shartning har ikkala tomoniga  $M$ -qovushoq-elastiklik operatoriga teskari  $M^{-1}$  operator bilan ta'sir etamiz. U holda

$$M^{-1}[\sigma_{r\theta}] - F'(z)M^{-1}[\sigma_{z\theta}] = \Delta M^{-1}[f_{nS_1}(z, t)],$$

$r = F(z)$  tenglamaga ega bo'lamiz.

Bu yerdan ko'rinadiki  $M^{-1}[\sigma_{r\theta}] - F'(z)M^{-1}[\sigma_{z\theta}] = \Delta M^{-1}[f_{nS_1}(z, t)]$  shartdan foydalanish uchun avvalo  $\sigma_{r\theta}$  va  $\sigma_{z\theta}$  larni kiritilgan yangi  $U_{\theta,0}^{(0)}$  funksiyaning originali bo'lgan  $U_{\theta,0}(z, t)$  funksiya orqali ifodalash kerak. Shu maqsadda  $U_{\theta,0}(z, t)$  funksiya va  $\lambda$ -operatorini quyidagicha kiritamiz

$$U_{\theta,0}(z, t) = \int_0^{\infty} \frac{\sin kz}{-\cos kz} \left. \right\} dk \int_{(l)} U_{\theta,0}^{(0)}(k, p) e^{pt} dp;$$

$$\lambda^n(U_{\theta,0}) = \int_0^{\infty} \frac{\sin kz}{-\cos kz} \left. \right\} dk \int_{(l)} \beta^{2n} U_{\theta,0}^{(0)}(k, p) e^{pt} dp.$$

Endi  $\sigma_{r\theta} = M \left[ \frac{1}{r} \frac{\partial}{\partial r} - \frac{\partial^2}{\partial r^2} \right] \Psi_1$ ,  $\sigma_{z\theta} = -M \frac{\partial^2 \Psi_1}{\partial r \partial z}$  formulalardan foydalanib

$\sigma_{r\theta}^{(0)}$  va  $\sigma_{z\theta}^{(0)}$  larni  $U_{\theta,0}^{(0)}$  orqali ifodalaymiz. Buning uchun ushbu

$$\sigma_{r\theta} = M \left[ \frac{1}{r} \frac{\partial}{\partial r} - \frac{\partial^2}{\partial r^2} \right] \Psi_1, \quad \sigma_{z\theta} = -M \frac{\partial^2 \Psi_1}{\partial r \partial z}. \text{ formulalarga}$$

$$\Psi_1(r, z, t) = \int_0^{\infty} \frac{\sin kz}{-\cos kz} \left. \right\} dk \int_{(l)} \Psi_1^{(0)}(r, k, p) e^{pt} dp \text{ va}$$

$$\sigma_{r\theta}(r, z, t) = \int_0^{\infty} \frac{\sin kz}{-\cos kz} \left. \right\} dk \int_{(l)} \sigma_{r\theta}^{(0)}(r, k, p) e^{pt} dp,$$

$$\sigma_{z\theta}(r, z, t) = \int_0^{\infty} \frac{\cos kz}{\sin kz} \left. \right\} dk \int_{(l)} \sigma_{z\theta}^{(0)}(r, k, p) e^{pt} dp, \text{ almashtirishlarni qo'llaymiz va mos}$$

ravishda quyidagilarni

$$\sigma_{r\theta}^{(0)}(r, k, p) = M_0 \left( \frac{1}{r} \frac{d}{dr} - \frac{d^2}{dr^2} \right) \psi_1^{(0)}(r, k, p),$$

$$\sigma_{z\theta}^{(0)}(r, k, p) = M_0 k \frac{\partial \psi_1^{(0)}(r, k, p)}{\partial r}.$$

Bu yerga  $\psi_1^{(0)}$  ning  $\Psi_1^{(0)}(r) = BI_0(\beta r)$  ifodasini qo'yamiz. U holda

$$\sigma_{r\theta}^{(0)}(r, k, p) = M_0 \left\{ \frac{2\beta}{r} [I_1(\beta r) - \beta^2 I_0(\beta r)] B \right\};$$

$$\sigma_{z\theta}^{(0)}(r, k, p) = -M_0 \left\{ k \left[ \beta I_0(\beta r) - \frac{1}{r} I_1(\beta r) \right] B \right\}.$$

Olingan ifodalarning har ikkala tomonlarini  $M_0^{-1}$  operatorni ta'sir ettiramiz

$$M_0^{-1} [\sigma_{r\theta}^{(0)}] = \frac{2\beta}{r} [I_1(\beta r) - \beta^2 I_0(\beta r)] B;$$

$$M_0^{-1} [\sigma_{z\theta}^{(0)}] = \left[ \frac{k}{r} I_1(\beta r) - k\beta I_0(\beta^2) \right] B.$$

Oxirgi formulalarning o'ng tomonlaridagi Bessel funksiyalarining o'rniga ularning darajali qatorlarga yoyilmalarini ishlatamiz va hosil qilingan ifodalarda  $B$ -o'zgarmas o'rniga uning  $U_{\theta,0}^{(0)} = -\frac{1}{2} \beta^2 B$  formula bilan aniqlanuvchi qiymatini

qo'yib  $\sigma_{r\theta}(r, z, t) = \int_0^{\infty} \frac{\sin kz}{-\cos kz} \left. \right\} dk \int_{(t)} \sigma_{r\theta}^{(0)}(r, k, p) e^{pt} dp,$

$$\sigma_{z\theta}(r, z, t) = \int_0^{\infty} \frac{\cos kz}{\sin kz} \left. \right\} dk \int_{(t)} \sigma_{z\theta}^{(0)}(r, k, p) e^{pt} dp, \text{ va}$$

$$U_{\theta,0}(z, t) = \int_0^{\infty} \frac{\sin kz}{-\cos kz} \left. \right\} dk \int_{(t)} U_{\theta,0}^{(0)}(k, p) e^{pt} dp;$$

$$\lambda^n (U_{\theta,0}) = \int_0^{\infty} \frac{\sin kz}{-\cos kz} \left. \right\} dk \int_{(t)} \beta^{2n} U_{\theta,0}^{(0)}(k, p) e^{pt} dp. \text{ almashtirishlarni}$$

qo'llaymiz.

Natijada

$$M^{-1} [\sigma_{r\theta}] = 2 \sum_{n=0}^{\infty} \frac{(r/2)^{2n+2}}{n!(n+1)!} \lambda^{n+1} U_{\theta,0};$$

$$M^{-1} [\sigma_{z\theta}] = 2 \sum_{n=0}^{\infty} \frac{(r/2)^{2n+1}}{n!(n+1)!} \lambda^n \frac{\partial U_{\theta,0}}{\partial z}.$$



ifodaga ega bo'lamiz. Ushbu qiymatlarni  $M^{-1}[\sigma_{r\theta}] - F'(z)M^{-1}[\sigma_{z\theta}] = \Delta M^{-1}[f_{nS_1}(z,t)]$ , chegaraviy shartga qo'yib izlanayotgan umumiy tenglamaga ega bo'lamiz:

$$\sum_{n=0}^{\infty} \frac{F^{2n+1}}{n!(n+1)!} \left[ \frac{F(z)}{2(n+2)} \lambda - F'(z) \frac{\partial}{\partial z} \right] \lambda^n U_{\theta,0} = [1 + F'^2(z)] M_0^{-1}[f_{nS_1}(z,t)]$$

Quyidagi olingan tenglamalar radiusi  $R = F(z)$  qonun bilan o'zgaruvchan, doiraviy qovushoq-elastik sterjenning buralma tebranish umumiy tenglamasidir. Bu tenglamadan xususiy holda quyidagi tenglamalar kelib chiqadi:

### XULOSA

a) Radiusi o'zgarmas, doiraviy, qovushoq-elastik sterjenning buralma tebranish umumiy tenglamasi.

Bu holda  $R = F(z) = const$  bo'lganligi uchun uni  $r_0$  orqali belgilaymiz, ya'ni

$$r_0 = R = F(z) = const,$$

u holda  $F'(z) = 0$  va demak

$$\Delta = 1 + F'^2(z) = 1,$$

Bundan tashqari  $(n, S_1, S_2)$  koordinat sistemasini bu holda kiritishga hojat yo'q, chunki  $\vec{n}$  normalni  $r, \theta, z$ -silindirik koordinat sistemasining  $r$ -radial o'qi bilan,  $S_1$  ni  $\theta$  koordinat o'qi bilan va  $S_2$  ni bo'ylama  $z$  koordinat o'qi bilan ustma-ust tushadi deb hisoblash mumkin. U holda  $f_{nS_1}(s_2, t)$  funksiyani  $f_{r\theta}(z, t)$  funksiya bilan almashtiramiz, ya'ni

$$f_{nS_1}(s_2, t) = f_{r\theta}(z, t).$$

Hosil qilingan  $r_0 = R = F(z) = const$ ,  $\Delta = 1 + F'^2(z) = 1$ , va  $f_{nS_1}(s_2, t) = f_{r\theta}(z, t)$ . tengliklarni, hamda  $F'(z) = 0$  ekanligini hisobga olsak

$$\sum_{n=0}^{\infty} \frac{F^{2n+1}}{n!(n+1)!} \left[ \frac{F(z)}{2(n+2)} \lambda - F'(z) \frac{\partial}{\partial z} \right] \lambda^n U_{\theta,0} = [1 + F'^2(z)] M_0^{-1}[f_{nS_1}(z,t)] \quad \text{dan}$$

izlanayotgan tenglamaga ega bo'lamiz.

$$\sum_{n=0}^{\infty} \frac{(r/2)^{2n+2}}{n!(n+2)!} \lambda^{n+1} U_{\theta,0} = M^{-1}[f_{r\theta}(z,t)]$$

bu yerda

$$\lambda^n = \left[ \frac{1}{b^2} M_0^{-1} \left( \frac{\partial^2}{\partial t^2} \right) - \frac{\partial^2}{\partial z^2} \right], \quad b^2 = \frac{\mu}{\rho}$$

b) Radiusi o'zgaruvchan, doiraviy, elastik sterjenning buralma tebranish umumiy tenglamalari.

Bu holda  $M = \mu$  deb hisoblash yetarli bo'ladi, ya'ni  $M = \mu M_0$ .

$$M[\zeta(t)] = \mu \zeta(t)$$

deb hisoblash yetarli. Agar  $M[\zeta(t)] = \mu \zeta(t)$  o'rinli bo'lsa

$$\lambda^n = \left[ \frac{1}{b^2} M_0^{-1} \left( \frac{\partial^2}{\partial t^2} \right) - \frac{\partial^2}{\partial z^2} \right], \quad b^2 = \frac{\mu}{\rho} \quad \text{quyidagicha yoziladi}$$

$$\lambda^n = \left[ \frac{1}{b^2} \left( \frac{\partial^2}{\partial t^2} \right) - \frac{\partial^2}{\partial z^2} \right]^n, \quad n = 0, 1, 2, \dots \quad b^2 = \frac{\mu}{\rho}$$

Demak, elastik sterjen uchun

$$\sum_{n=0}^{\infty} \frac{F^{2n+1}}{n!(n+1)!} \left[ \frac{F(z)}{2(n+2)} \lambda - F'(z) \frac{\partial}{\partial z} \right] \lambda^n U_{\theta,0} = [1 + F'^2(z)] M_0^{-1} [f_{nS_1}(z, t)] \quad \text{tenglamaning}$$

umumiy ko'rinishi saqlanadi, ya'ni

$$\sum_{n=0}^{\infty} \frac{F^{2n+1}(z)}{n!(n+1)! 2^{2n}} \left[ \frac{F(z)}{2(n+2)} \lambda - F'(z) \frac{\partial}{\partial z} \right] \lambda^n U_{\theta,0} = [1 + F'^2(z)] f_{nS_1}(s_2, t),$$

bu yerda  $\lambda - \lambda^n = \left[ \frac{1}{b^2} \left( \frac{\partial^2}{\partial t^2} \right) - \frac{\partial^2}{\partial z^2} \right]^n, \quad n = 0, 1, 2, \dots \quad b^2 = \frac{\mu}{\rho}$  formula bilan

hisoblanishi zarur.

c) Radiusi o'zgarmas, doiraviy, elastik sterjenning buralma tebranish umumiy tenglamalari.

Bu holda xuddi a) holatdagidek  $r_0 = R = F(z) = const$ ,  $\Delta = 1$ ,  $F'(z) = 0$  deb

hisoblasak hamda  $f_{nS_1}(s_2, t) = f_{r\theta}(z, t)$ . tenglikni e'tiborga olsak

$$\sum_{n=0}^{\infty} \frac{F^{2n+1}(z)}{n!(n+1)! 2^{2n}} \left[ \frac{F(z)}{2(n+2)} \lambda - F'(z) \frac{\partial}{\partial z} \right] \lambda^n U_{\theta,0} = [1 + F'^2(z)] f_{nS_1}(s_2, t) \quad \text{tenglama quyidagi ko'rinishni oladi.}$$

$$\sum_{n=0}^{\infty} \frac{F^{2n+1}(z)}{n!(n+1)! 2^{2n}} \lambda^{n+1} U_{\theta,0} = \frac{1}{\mu} f_{r\theta_1}(r, z)$$

bu yerda  $\lambda^n, n = 0, 1, 2, \dots$  operatorlar

$$\lambda^n = \left[ \frac{1}{b^2} \left( \frac{\partial^2}{\partial t^2} \right) - \frac{\partial^2}{\partial z^2} \right]^n, \quad n = 0, 1, 2, \dots \quad b^2 = \frac{\mu}{\rho} \quad \text{formula bilan}$$

hisoblanishi kerak.



## REFERENCES

1. мензаде Ю.А. Теория упругости. – М: Высшая школа, 1996. – 272с.
2. Болотин В.В. Колебания и устойчивость упругой цилиндрической оболочки в потоке сжимаемого газа // . Сборник. – 1976. – 24.-С.3-16.
3. Ляв А. Математическая теория упругости. – М. – Л.: ОНТИ, 1935. – 674с.
4. Никифоров А.Ф., Уварова В.Б. Специальные функции математической физики. – М. «Наука», 1998. – 320с.
5. Петрашень Г.И. Проблемы инженерной теории колебаний вырожденных систем // Исследования по упругости и пластичности.- Л.:»Изд-во ЛГУ», 1996. №5.-С. 3-33.
6. Филиппов И.Г., Худойназаров Х.Х. Уточнение уравнений продольно-радиальных колебаний круговой цилиндрической вязкоупругой оболочки // Прикл. мех.-1990.-26,№2.-с.63-71.
7. Филиппов И.Г., Чебан В.Г. Математическая теория колебаний упругих и вязкоупругих пластин и стержней. – Кишнев: «Штиинца», 1998. – 190с.
8. Худойназаров Х.Х. Нестационарное взаимодействие круговых цилиндрических упругих и вязкоупругих оболочек и стержней с деформируемой средой. – Ташкент: «Изд-во им. Абу Али ибн Сино», 2003.- 325с.
9. Xudoyberdiyev, S. I., Ashurov, B. I., Khudoyberdiyev, S. I., & Ashurov, B. I. (2021). QOVUSHOQ-ELASTIK STERJENDA TEBRANISH JARAYONIDA REZONANS HOSIL BO'LISHI. *Academic research in educational sciences*, 2(3).